

MICROCOPY RESOLUTION TEST CHART NATIONAL BUREAU OF STANDARDS-1963-A





U.S. Department of Transportation Federal Autation

Office of Environmental and Energy Washington, D.C. 20591

## FAA/GAMA Propeller Aircraft Noise Test Program Salina Municipal Airport Salina, Kansas

AD-A154 818



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## FAA/GAMA PROPELLER AIRCRAFT NOISE TEST PROGRAM

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## I. INTRODUCTION

In September, 1984, the Federal Aviation Administration, with the cooperation and support of the General Aviation Manufacturers Association, conducted a noise measurement program on propeller-driven aircraft at Salina Municipal Airport, Salina, Kansas. The program objectives were:

- (1) to measure the benefits of noise abatement takeoff

  procedures being developed by the manufacturers for

  inclusion in the Pilot's Operating Handbook, and
- (2) to obtain takeoff noise data using proposed ICAO Annex
  16 and FAR Part 36 certification procedures for
  propeller-driven small airplanes.

ICAO and FAA noise standards prescribe procedures for noise certification of small propeller-driven airplanes. The standards require measurement of the noise levels resulting from level flyovers at 1000' at not less than the highest power in the normal operating range. The regulations also require application of an aircraft performance correction based on the aircraft's climb performance and the associated effect on noise levels.

Proposed changes to Chapter 6 of ICAO Annex 16 and FAR Part

36 Appendix F would substitute a takeoff test for the current

flyover procedures. For the Salina takeoff tests, the flight

procedures (using maximum continuous installed power), general test conditions, measurement equipment and procedures, and data adjustments to correct for off-reference test conditions were in accordance with the proposed regulatory changes. Where appropriate, the measurements and data adjustments for the reduced power takeoffs were also in accordance with the proposed changes.

## II. TEST LOCATION

Salina Municipal Airport was selected because of its low ambient noise level, the availability of a runway dedicated to the tests and the proximity of the airport to the home field of many of the aircraft. The test aircraft used runway 12 with a right hand race track pattern. Figure 1 shows the flight track overlaid on an airport obstruction chart, Also shown on Figure 1 are the noise measurement and photographer sites and the location of the aircraft rotation point. A detailed description of the aircraft sontained in the master airport record dated September 15, 1983, appended as Attachment A.

## III. FLIGHT PROCEDURES

A. The noise measurement point is required to be on the extended centerline of the runway at a distance of 8200 feet (2500m) from the start of takeoff roll. However, by using flight path intercept procedures, the noise measurements were made on a grassy area about 50 feet abeam runway 12-30 at about midfield. In order for a test run to be acceptable, the aircraft

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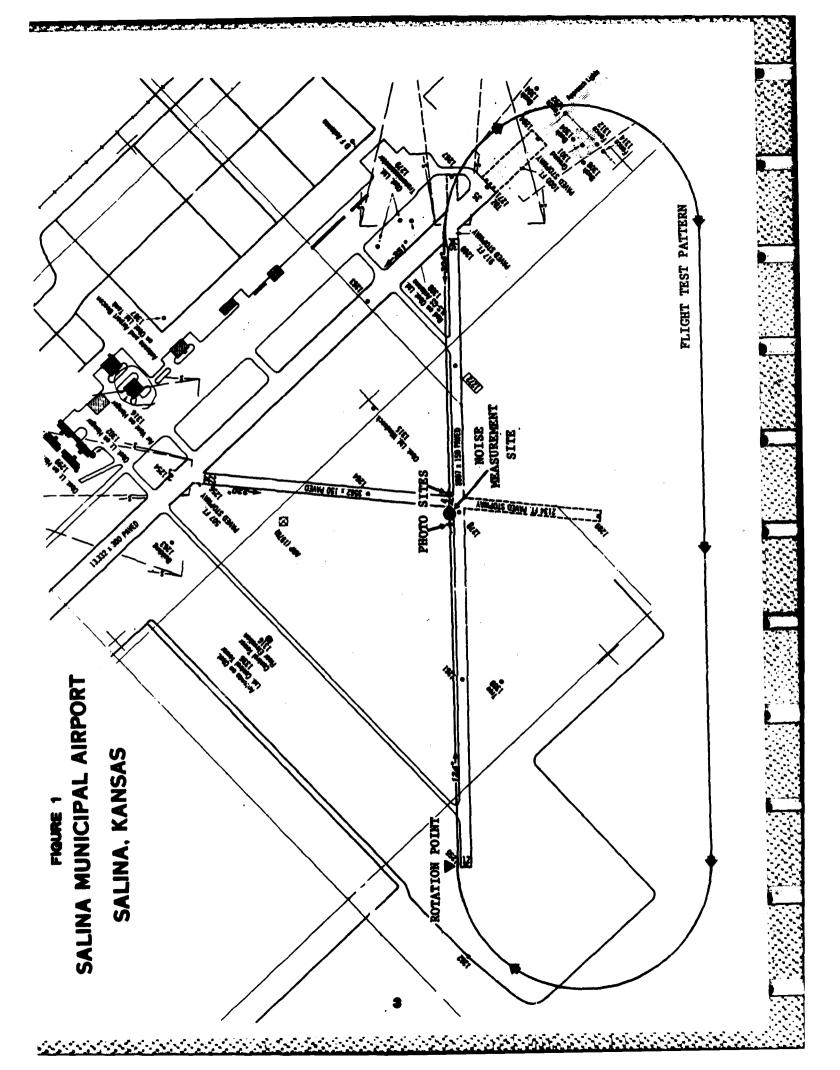
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were required to pass over the measurement point within  $\pm$  10 degrees from the vertical and within 20% of the reference altitude.

- B. The reference altitudes were calculated for the following atmospheric conditions:
  - (1) Sea level atmospheric pressure of 1013.25 mb,
  - (2) Ambient air temperature of 59°F (15°C)
  - (3) Relative humidity of 70 percent, and
  - (4) Zero wind.
  - C. The takeoff reference altitudes for the proposed certification procedure were calculated by the manufacturer assuming the following two segments:
    - (1) First segment.
      - (a) Takeoff power from the brake release point to the point at which the height of 50 feet (15m) above the runway is reached.
        - (b) A constant takeoff configuration selected by the applicant was maintained through this segment.
        - (c) The length of the first segment corresponded to the airworthiness approved value for a takeoff on a level paved runway.
    - (2) Second Segment.
      - (a) The beginning of the second segment corresponds to the end of the first segment.
      - (b) Each airplane was in the climb configuration with landing gear up and flap setting

corresponding to normal climb procedures throughout the second segment.

- (c) In each case, the aircraft velocity was the speed for best rate of climb,  $\mathbf{V}_{\mathbf{v}}$ .
- (d) Maximum continuous installed power and rpm were maintained throughout the second segment.
- (3) Tests using these procedures were designated the "A" series.
- D. The manufacturer of each test aircraft described a reduced power takeoff procedure and calculated the reference altitude at 8200 feet from the start of takeoff roll at maximum takeoff gross weight under the atmospheric conditions specified in Section IIIB. In general, the procedures used maximum continuous power to 500 feet above ground level, then power was reduced to 75% of maximum continuous with the lowest rpm consistent with that power to continue climbing over the measurement site. Tests using these procedures were designated the "B" series.
- E. The Piper Seneca III was also tested using a maximum power rating limited to five minutes. The takeoff reference altitude for this series (designated "C") was calculated using the procedure described in Section IIIC.

## IV. Data Acquisition

- A. Acoustical Data.
  - (1). The terrain in the vicinity of the measurement location was relatively flat with no obstructions within a conical space above the measurement

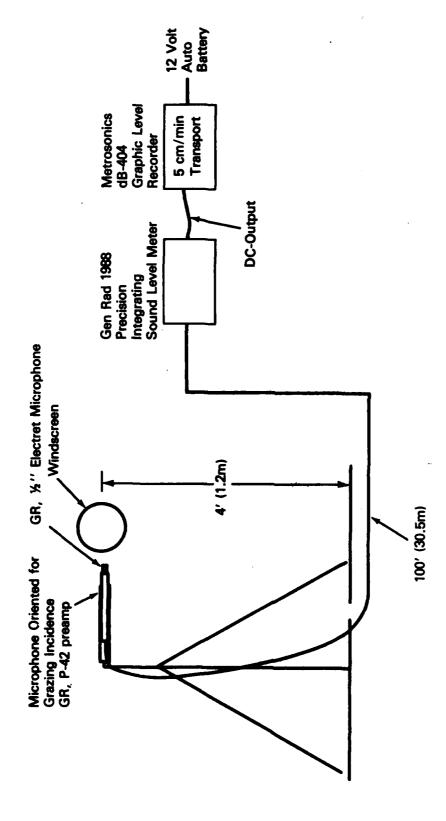
position, the cone defined by an axis normal to the ground and by a half-angle 75° from the axis. The grass was moved to a height of about two inches. (2) The measurement site was located 50 feet abeam of runway 12-30 at a point 5000' from the threshold of runway 12. As flight path intercept procedures were used, this site represented 8200' from start of takeoff roll as required by the proposed regulation. (3) Two identical microphone preamp systems situated 12 inches apart were used at the measurement site. Each system consisted of a General Radio 1/2 inch electret microphone (1962-9610) driving P-42 preamplifiers, with the microphones oriented for grazing incidence at four feet above the ground. Three inch windscreens were used throughout the tests. A 100-foot cable connected each microphone system to a General Radio 1988 Precision Integrating Sound Level Meter (PISLM). One of the GR 1988 PISLMs drove a Metrosonics Graphic Level Recorder. The acoustics data acquisition setup is shown in schematic form on Figure 2, whereas the measured and corrected acoustical data are listed in Section VIII.

## B. Aircraft Position Data.

(1) Aircraft position relative to the reference flight profile and the noise measurement site was determined by scaling photographs taken of the aircraft as it

FIGURE 2

# Acoustical Measurement Instrumentation



Direct Read Noise Measurement System

passed over cameras located along the flight track 100 feet before and 185 feet past the noise measurement site. The altitudes calculated were averaged (with proper weighting) to obtain the altitude over the microphones. A polaroid camera was used to determine in situ whether or not the aircraft was within the test window (±20% of the reference altitude and ±10° from the azimuth). Acceptable data from at least six overflights were required to insure a statistically valid average sound level. Further, the variation in these flights had to be such that the 90% confidence level did not exceed 1.5 decibels.

## C. Meteorological Data.

(1) Wind direction and velocity at ten meters above ground were recorded for each run. Relative humidity and temperature at ground level were recorded every 15 minutes throughout the tests. These data are tabulated in Appendix A.

## D. Aircraft Flight Data.

- (1) For each test run, an FAA observer recorded the manifold pressure or torque, propeller rpm, indicated airspeed, altitude over the noise measurement site and the outside air temperature.
- (2) A videotape record was made of the instrument panel during each test run. Data from these tapes are presented in Appendix B.
- (3) Tachometer checks using a view-thru tachometer were made on each test aircraft.

## TABLE VIII

## FAA/GAMA PROPELLER AIRCRAFT NOISE PROGRAM

## SALINA,KS FIELD ELEVATION 1270'

AIRCRAFT: MOONEY 201

TEST DATE: 9/18/84

REFERENCE ALTITUDE: 790'

EVENT	MEAS.ALT AGL(ft)	NOISE LVL dBA(MEAS)	DELTA(M)	DELTA(1)	DELTA(2)	DELTA(3)	NOISE LVL dBA(CORR)
A56	793	76.55	.16	.04	.58	.62	77.95
A57	702	76.35	.14	-1.13	.58	.6	76.54
A58	721	76	.14	87	.66	.62	76.55
A61	749	76.9	.15	51	.66	.63	77.83
A62	717	76.4	.14	93	.66	.62	76.89
A64	838	76.35	.17	.56	. 66	.62	78.36
					A	JERAGE>>	77.35
					s.	TD DEV>>	0.79
					9(	ox c.i.>	0.45

AIRCRAFT: MOONEY 201

TEST DATE: 9/18/84

REFERENCE ALTITUDE 645.00 W/REDUCED POWER

EVENT	MEAS.ALT AGL(ft)	NOISE LVL dBA(MEAS)		DELTA(1)	DELTA(2)	DELTA(3)	NOISE LVL dBA(CORR)
866	677.00	72.45	0.13	0.46	0.65	0.00	73.69
B71	648.00	73.10	0.13	0.04	0.65	0.00	73.92
874	<b>681.00</b>	71.75	0.14	0.52	0.65	0.00	73.06
B7.6	641.00	72.75	0.13	-0.06	0.65	0.00	73.47
B77	690.00	71.70	0.14	0.64	0.65	0.00	73.13
B78	685.00	71.50	0.14	0.57	0.65	0.00	72.86

AVERAGE>> 73.36 STD DEV>> 0.41 90% C.I.> 0.33

## TABLE VII

## FAA/GAMA PROPELLER AIRCRAFT NOISE PROGRAM

## SALINA,KS FIELD ELEVATION 1270'

AIRCRAFT: SENECA III

TEST DATE: 9/18/84

REFERENCE ALTITUDE 928'

EVENT		NOISE LVL	DELTA(M)	DELTA(1)	DELTA(2)	DELTA(3)	NOISE LUL dba(corr)
A37 A38 A39 A40 A41 A42	877 <b>955</b> <b>9</b> 26 962 1024 993	78.35 78.55 78 78.7 80 77.9	0 0 0	54 .27 0 .34 .94	.14 .14 .06 .14 .14	.04 .04 .04 .04 .04	77.99 79.00 78.10 79.22 81.12 78.83
					en St	VERAGE>>  TD DEV>>  D% C.I.>	79.04 1.13

AIRCRAFT: PIPER SENECA 111

TEST DATE: 9/18/84

REFERENCE ALTITUDE 713.00 W/REDUCED POWER

EVENT	MEAS.ALT AGL(ft)		DELTA(M)	DELTA(1)	DELTA(2)	DELTA(3)	NOISE LVL
B47 B48 B49 B50 B51 B52	729.00 708.00 805.00 709.00 721.00 715.00	74.20 74.20 73.65 75.10 73.85 74.45	0.00 0.00 0.00 0.00 0.00	0.21 -0.07 1.16 -0.05 0.11 0.03	0.18 0.18 0.18 0.18 0.18	0.00 0.00 0.00 0.00 0.00	74.59 74.31 74.99 75.23 74.14 74.66
						VERAGE>>	74.65 0.41

AIRCRAFT: SENECA III

TEST DATE: 9/19/84

90% C.I.> 0.33

REFERENCE ALTITUDE: 1014'

EVENT		NOISE LUL	DELTA(M)	DELTA(1)	DELTA(2)	DELTA(3)	NOISE LVL dBA(CORR)
C26	919	81.85	.18	94	.95	.22	82.26
C27	990	80.9	.2	-,23	.95	.22	82.04
C28	1016	81.25	.2	0	.95	.22	82.62
C29	783	82.7	.2	3	.95	.22	B3.77
C30	1094	79.65	.22	.73	. 95	.22	81.77
C31	748	81.35	.19	64	.75	.22	82.07
					A	JERAGE>>	82.42
					8	TD DEV>>	0.72
					91	0% C.I.>	0.59

## TABLE VI

## FAA/GAMA PROPELLER AIRCRAFT NOISE PROGRAM

## SALINA,KS FIELD ELEVATION 1270'

AIRCRAFT: MOONEY 231

TEST DATE: 9/18/84

REFERENCE ALTITUDE 778'

	MEAS.ALT	NOISE LVL					NOISE LUL
EVENT	AGL(ft)	dBA(MEAS)	DELTA(M)	DELTA(1)	DELTA(2)	DELTA(3)	dBA(CORR)
A23	715	78.7	0	81	0	08	77.81
A24	669	79.15	Ŏ	-1.44	Ŏ	08	77.63
A25	837	77.2	0	.7	Ö	08	77.82
A26	827	77.35	0	.58	0	08	77.85
A27	836	77.35	0	.69	0	08	77.96
A28	827	77.35	0	.58	0	08	77.85
					A	JERAGE>>	77.82
					S	TD DEV>>	0.11
					9	0% C.I.>	0.09

AIRCRAFT: MOONEY 231

TEST DATE: 9/18/84

REFERENCE ALTITUDE

643 W/REDUCED POWER

EVENT	AGL(ft)	ADA/MEADA					NOISE LVL
		dBA(MEAS)	DELTA(M)	DELTA(1)	DELTA(2)	DELTA(3)	dBA(CORR)
					~		
829	675	74.05	0	0.46	0	0	74.51
B30	616	75.25	0	-0.41	0	0	74.84
B31	651	74.1	0	0.12	0	0	74.22
B32	592	74.65	0	-0.79	0	0	73.86
B33	758	73.2	0	1.57	0	0	74.77
B34	730	72.6	0	1.21	0	0	73.81

AVERAGE>> 74.34 STD DEV>> 0.45 90% C.I.> 0.37

## TABLE V

## FAA/GAMA PROPELLER AIRCRAFT NOISE PROGRAM

## SALINA,KS FIELD ELEVATION 1270'

AIRCRAFT: BEECH A-36

TEST DATE: 9/18/84

REFERENCE ALTITUDE 753'

EVENT	MEAS.ALT AGL(ft)		DELTA(M)	DELTA(1)	DELTA(2)	DELTA(3)	NOISE LVL dBA(CORR)
A6	869	81.9	0	1.37	.2	0.60	84.07
A7	784	82	0	.39	.2	0.58	83.17
A8	793	80.55	0	.49	.2	0.58	81.82
A9	899	80.6	0	1.69	.2	0.61	83.10
A10	798	81.35	0	.55	.12	0.58	82.60
					A	/ERAGE>>	82.95
					S	ID. DEV>	0.83
					90	0% C.I.>	0.79

AIRCRAFT: BEECH A-36

TEST DATE: 9/18/84

REFERENCE ALTITUDE # 625 W/REDUCED POWER

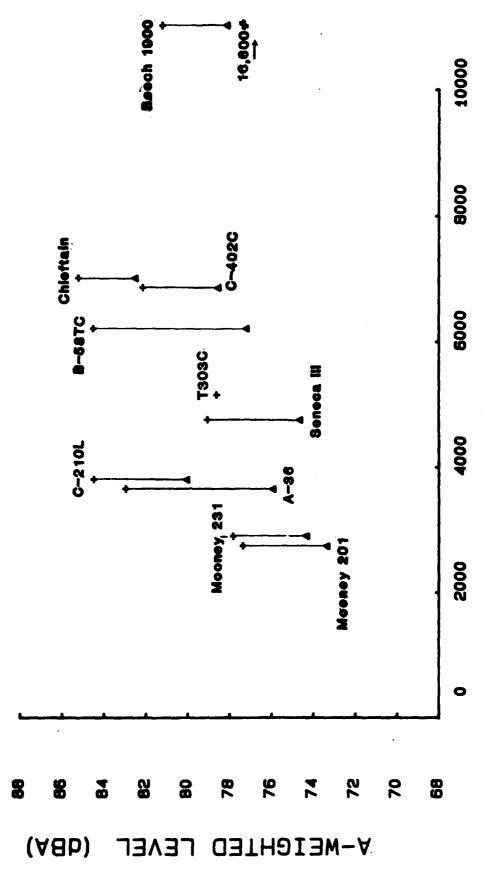
EVENT		NOISE LVL	DELTA(M)	DELTA(1)	DELTA(2)	DELTA(3)	NOISE LVL dBA(CORR)
B11	597	76.3	0	-0.44	.09	0	75.95
B12	678	75.05	0	0.78	.09	0	75.92
813	718	73.95	0	1.33	.09	0	75.37
B14	684	74.45	0	0.86	.09	0	75.40
815	766	73.8	0	1.94	.09	0	75.83
B16	759	74.85	0	1.86	.09	0	76.80
817	715	74.9	0	1.29	.09	0	76.28
					A	VERAGE>>	75.93
					S	TD DEV>>	0.50
					9	0% C.I.>	0.37

## VIII. MEASURED AND CORRECTED DATA:

Tables V through XIV present the "as measured" noise levels and airplane altitude over the measurement point for each data run. To these noise levels are added the adjustments shown in the tables for off-reference meteorological conditions, Delta (M); altitude, Delta (1); helical tip Mach number, Delta (2); and engine power, Delta (3) to obtain the corrected noise levels shown.

Table XV presents the data used in calculating the off-reference power correction, Delta (3) for airplanes with normally aspirated engines (the beech A-36, the Mooney 201 and the Cessna 210L).

PROPELLER DRIVEN SMALL AIRPLANE TAKEOFF NOISE LEVELS



TAKEOFF GROSS WEIGHT (LB)

17

throughout the test run. The noise level over the measurement site for this series averaged 82.42 dBA, 3.38 dB more than with maximum continuous power and 7.77 dB over the level when the reduced power procedures were used.

The data presented in Table IV are shown in graphical form on Figure 3.

TABLE IV

## FAA/GAMA PROPELLER AIRCRAFT NOISE PROGRAM

## TAKEOFF NOISE LEVELS

	CERT LEVEL	REDUCED POWER	
AIRCRAFT	VEP	dBA	DELTA dBA
BEECH A-36	82.95	75.93	7.0
MOONEY 231	77.82	74.34	ທ. ຕ
SENECA III	79.04	74.65	₩.
HOONEY 201	77.35	73.36	0
CESSNA 210L	84.49	90 . 08	•
BEECH SOTC	84. A9	77.20	2.3
CESSNA T303	98.59	ı	ı
BEECH 1900	81.16	78.10	. u
CESSNA 402C	82.12	78.54	9 · 6
PIPER CHIEFTAIN	65.18	82.49	2 . 7

data at other Mach numbers would be required to determine an approved value for k for each aircraft.

E. Measured sound levels were adjusted for engine power by algebraically adding an increment equal to:

Delta (3) = 17 Log  $(P_R/P_T)$ 

where  $P_{\overline{I}}$  and  $P_{\overline{R}}$  are the test and reference engine powers, respectively.

For all of the tests at maximum continuous power (and maximum takeoff power for the Seneca III), an off-reference temperature correction equal to the square root of the ratio of the absolute temperatures,  $(T_{\rm ref.std.atmo.}/T_{\rm test})^{\frac{1}{2}}$ , was applied to obtain the test engine power. For normally aspirated engines, the following additional correction, taken from NACA Report No. 654 entitled "General Airplane Performance," was used to calculate  $P_{\rm T}$ :

HPAlt. = HPSea Level  $(\sigma - 0.017)/0.883$  where  $\sigma$  = air density ratio.

These calculations are presented in Section VIII.

## VII. Test Results

Table IV lists the fully corrected noise levels for the ten aircraft tested in accordance with the proposed certifications and the nine tested using reduced power. The noise reduction achieved by reducing from maximum continuous power to about 75% power with a lower propeller rpm varied from about 3 to over 7 decibels with an average noise reduction of 4.4 decibels. The Seneca III was also tested at maximum takeoff power

TABLE III

FAA/GAMA PROPELLER AIRCRAFT NO.1SE PROGRAM

## HELICAL TIP MACH NUMBER CORFFICIENTS

	. A . SERIES	REDUCED POWER	TIP MACH NO.
AIRCRAFT	TIP MACH NO.	TIP MACH NO.	COMP. (M)
\$ ? B ? B 1 6 8			
BEECH A-36	0.835	75.93	198
HOONEY 231	0.797	74.34	10 <b>0</b>
SENECA 111	0.783	0.724	142
HOONEY 201	0.784	0.700	78
CESSNA 210L	• • •	0.752	<b>6</b>
BEECH SOTC	9 · 0	0.739	145
CESSNA T303	1	•	•
BENCH 1900	0.745	0.683	7.1
CESSNA 401C	0.814	0 . 7 4 3	102
PIPER CHIEFTAIN	208.0	0.753	102
SENECA III	0.783	0.831.4	105
		AVERAGE	H 103

\* MAX. TAKEOFF POVER

where: H<sub>T</sub> is the height in feet of the test aircraft over the measurement point, and Q'is the rate of absorption for test day conditions at 500 Hz specified in the Society of Automotive Engineer's Aeronautical Recommended Practice #866A entitled"Standard Values of Atmospheric Absorption as a Function of Temperature and Humidity for Use in Evaluating Aircraft Flyover Noise."

C. The measured sound levels were adjusted for offreference altitude by algebraically adding an increment equal
to:

Delta (1) = 22 Log ( $H_T/H_R$ ) where:  $H_T$  is as defined above, and  $H_R$  is the reference height of the aircraft over the measurement point.

D. For test runs where the test helical tip Mach number  $(M_T)$  was smaller than the reference helical tip Mach number  $(M_R)$ , the measured sound levels were adjusted by algebraically adding an increment equal to:

Delta (2) = k Log  $(M_R/M_T)$ 

where the constant k was assigned the nominal value of 150 allowed in the proposed regulations when  ${\rm M}_{\rm T}$  is smaller than  ${\rm M}_{\rm p}$  .

For those aircraft tested at two propeller rpms, values of k
were calculated and are listed in Table III. It must be
emphasized that these constants were calculated from only two
nominal values of helical tip Mach numbers and that additional

TABLE II

PAA/GAMA PROFELLER AIRCRAFT MOISE PROGRAM

## REFERENCE TAKEOFF CONDITIONS

		SEA LEV	SEA LEVEL STANDARD DAY	RD DAY	MCP CA	HCP (A Series)	REDUCED POWER (B Series)	POWER (	200	
AIBCRAFT	MAK GROSS T/O UT(188)	T/O DIST To S0 ((t)	Vy (Kts)	MAX CLIMB MATE(ft/min)	MEF	REF ALT	T WE W	MA II	REF ALT	ן ן
36 ECH A-34	9876	3 2 0 0	0	1160	0.8576	753	2 + 0 0	0.7655	\$ 7 9	
MOCHET 131	3.00	1750	*	1040	0.7740	7.85	3400	0.7091	;	_
SENECA 111		1650	8	1275	0.7847	123	3400	0.7243	713	
M6CHERY 201	3740	•••1	:	1940	0.7720	789	2400	0.7048	. •	
CESSWA 310	•	3030	*	0 #	9.8564	989	3404	0.7643	619	
BESCH SOTC	• • • • • • • • • • • • • • • • • • • •	1828	. 811	00 7 1	0.8413	0.00	3400	0.7530	•	
CESSMA TIO	9 1 2 9	1780		1.00	0.7114	978	•	1	:	
BESCH 1989	16600	•	138	0000	0.7556	9 8	1550	0.440	7	_
CESSERA 403	• • • • • • • • • • • • • • • • • • • •	21.95	100		0.8239	888	9576	0.7508	•••	
IPER CHIBETAIN	1H 7000	2700	. 101	1400	0.8175	910	7 400	9.7658	Š	

TABLE 1

SECON PROBLEM SECONDS

## FAA/GAMA PROPELLER AIRCRAFT NOISE PROGRAM

## AIRCRAFT SPECIFICATIONS

			ENCINE	DATA			124	PROPELLER DATA	R DATA			
AIRCRAFT	MODEC	7. 9.1	NUMBER	MAXCONT	e K	AIR	HODEL	NUMBER	UIA (Inch.)	PITCH F/V	SPAN	CRAR 7/R
BEECH A-36 BOMANZA	CONTINENTAL IO-550-8	PISTON	<del></del>	0 0 0	2700	NORM. Aspri.	Mecaulry	•	:	>		•
MOONEY 231. M26K	Continental TSIO-340-GB	FISTON	<b></b>	210	2700	TURBO	McCAULEY	•	2	>	:	<b>≪</b>
PIPER PAS4-220T SENECA III	CONTINENTAL TSIO-340	PISTON	M	200	9 9 8	TURBO	McCAULEY	M	2	>	. 11 00	*
HOONEY 101 H165	LYCOMING LYCOMING	FISTON	-	300	2700	Norm. Aspir.	McCAULEY	м		>	:	•
CESSNA 210C CENTURIAN	CONTINENTAL 10-528-L	P1STON	<b>~</b>	<b>8</b>	3 7 0 0	NORM.	McCAULEY	•	•	>	: : :	*
WERCH SATC	CONTINENTAL TSIO-520-VB	FISTON	M	818	100	TURBO	RECAULET	•	2	>	37.10"	•
CESSNA T303 CRUSADER	Continental TS10-520-AE	FISTON	•	250	9 7 7	TURBO	McCAULEY	•		>		
BEECH 1900 AIRLINER	PT6A-65B	TURBOFROF	•	1100	1700	TURBINE	HARTZELL	•	109.8	>		<b>«</b>
CESSNA 402C Busineseliner	Continental T810-510-ve	Notaif	*	8 8 8	3700	TURBO	McGAULEY	•	<b>36</b> . <b>3</b>	>		*
FIPER PA31-350 CHIEFTAIN	LYCOMING TSIO-546-J280	PISTON	•	o 99	2575	TVRBO	HARTZELL	•	•	>	: • •	€

## V. Aircraft Specifications

Table I presents selected physical characteristics for each of the test aircraft while Table II lists the reference takeoff performance values for each airplane.

## VI. Data Adjustment

A. Adjustments to the measured data tabulated in Section VIII were made in accordance with the proposed regulatory changes to account for the effects of:

- (1) Differences in atmospheric absorption between meteorological test conditions and reference conditions.
- (2) Differences in the noise path length between the actual airplane flight path
- (3) The change in the helical tip Mach number between test and reference conditions.
- (4) The change in engine power between test and reference conditions
- B. No correction for atmospheric absorption was required if the tests were conducted within the "no correction" window (temperature between 50 and 95°F and relative humidity between 45 and 95 percent). The temperature was within the "no correction" window for all of the data runs but the relative humidity was below 45% for nearly one-half of the tests. For these, the measured sound levels were adjusted from test day meteorological conditions to reference conditions by adding an increment equal to:

Delta (M) =  $(Q - 0.7)H_T/1000$ 

TABLE IX

## FAA/GAMA PROPELLER AIRCRAFT NOISE PROGRAM

## SALINA,KS FIELD ELEVATION 1270'

AIRCRAFT: CESSNA 210L

TEST DATE: 9/18/84

pのでは、「「「「なったのなない」となるななななな。「あったなななななな。」ということ、「「あまないのできない」「ますってきなるとう

REFERENCE ALTITUDE: 656'

EVENT		NOISE LVL dBA(MEAS)	DELTA(M)	DELTA(1)	DELTA(2)	DELTA(3)	NDISE LVL dBA(CORR)
A80	714	83.05	.14	.81	.97	.65	85.62
A81	724	82.2	.14	.94	.97	.65	84.90
A83	553	83.5	.11	-1.63	.97	.61	83.56
A84	736	81.45	.15	1.1	.97	.66	84.33
A85	672	82.45	.13	.23	.97	.64	84.42
A86	675	82	.13	.27	1.04	. 65	84.09
					A	VERAGE>>	84.49
					s	TD DEV>>	0.71
					9	0% C.I.>	0.58

AIRCRAFT: CESSNA 210L

TEST DATE: 9/18/84

REFERENCE ALTITUDE

616.00 W/REDUCED POWER

EVENT"		NOISE LVL dBA(MEAS)	DELTA(M)	DELTA(1)	DELTA(2)	DELTA(3)	NOISE LVL dBA(CORR)
887	643.00	78.35	0.13	0.41	0.94	0.00	<i>79</i> .83
B88	697.00	77.90	0.14	1.18	1.03	0.00	80.25
B89	601.00	79.70	0.12	-0.24	1.03	0.00	80.61
B90	693.00	77.65	0.14	1.13	1.03	0.00	79.95
B91	523.00	80.30	0.10	-1.56	1.03	0.00	79.87
B92	713.00	77.40	0.14	1.40	0.94	0.00	79.88

AVERAGE>> 80.06 STD DEV>> 0.31 90% C.1.> 0.26

TABLE X

## FAA/GAMA PROPELLER AIRCRAFT NOISE PROGRAM

## SALINA,KS FIELD ELEVATION 1270'

	F	T AA/GAMA PR NOIS	GABLE X ROPELLER A	IRCRAFT				
		SA	LINA,KS					
AIRCE	RAFT: BEECH		.EVATI <b>O</b> N 1 'C		EST DATE:	9/18/84		
	ERENCE ALT							
ENT	MEAS.ALT	NOISE LVL dBA(MEAS)	DELTA(M)	DELTA(1)	DELTA(2)	DELTA(3)	NOISE LVL dBA(CORR)	
93 94 95 96 97	871 952 862 991 961 832	81.9 80.3 83.95 81.1 82.1 81.6	.17 .19 .17 .2 .19	.38 1.23 .28 1.61 1.32	1.43 1.43 1.43 1.43 1.35	.27 .27 .27 .27 .27 .27	84.15 83.42 86.10 84.61 85.23 83.41	
					A	/ERAGE>>	84.49	
					ST	TD DEV>>	1.06	
					90	% C.I.>	0.87	
	RAFT: BEECH FERENCE ALT MEAS.ALT	TITUDE	<b>685.00</b>	T w/REDUCED	EST DATE:			
	FERENCE ALT	NOISE LVL dBA(MEAS) 73.70 75.55 74.90 74.45	685.00	w/REDUCED	POWER  DELTA(2)  1.14 1.22 1.14	9/18/84	0.87  NOISE LVL dBA(CORR)  76.81 78.09 77.65 76.57 77.11 76.98	
RE 00 01 03 04	FERENCE ALT MEAS.ALT AGL(ft)  827.00 774.00 797.00 747.00 593.00	NOISE LVL dBA(MEAS)  73.70 75.55 74.90 74.45 77.15	0.17 0.17 0.15 0.16 0.15 0.12	W/REDUCED  DELTA(1) 80  1.17  1.45  0.83  -1.38	POWER  DELTA(2)  1.14 1.22 1.14 1.14 1.22 1.22	9/18/84  DELTA(3)  0.00 0.00 0.00 0.00 0.00	NOISE LVL dBA(CORR)  76.81 78.09 77.65 76.57 77.11	
RE VENT 100 101 103 104	FERENCE ALT MEAS.ALT AGL(ft)  827.00 774.00 797.00 747.00 593.00	NOISE LVL dBA(MEAS)  73.70 75.55 74.90 74.45 77.15	0.17 0.17 0.15 0.16 0.15 0.12	W/REDUCED  DELTA(1) 80  1.17  1.45  0.83  -1.38	DELTA(2)  1.14 1.22 1.14 1.22 1.14 1.22	9/18/84  DELTA(3)  0.00 0.00 0.00 0.00 0.00	NOISE LVL dBA(CORR)  76.81 78.09 77.65 76.57 77.11	

EVENT		NOISE LVL dBA(MEAS)	DELTA(M)	DELTA(1)	DELTA(2)	DELTA(3)	NOISE LVL
B100	827.00	73.70	0.17	80	1.14	0.00	76.81
B101	774.00	75.55	0.15	1.17	1.22	0.00	78.09
B103	797.00	74.90	0.16	1.45	1.14	0.00	77.65
B104	747.00	74.45	0.15	0.83	_ 1.14	0.00	76.57
B105	593.00	77.15	0.12	-1.38	1.22	0.00	77.11
B106	806.00	74.05	0.16	1.55	1.22	0.00	76.98

## TABLE XI

## FAA/GAMA PROPELLER AIRCRAFT NOISE PROGRAM

## SALINA,KS FIELD ELEVATION 1270'

AIRCRAFT: CESSNA T303

TEST DATE: 9/19/84

REFERENCE ALTITUDE: 975'

EVENT		NOISE LVL	DELTA(M)	DELTA(1)	DELTA(2)	DELTA(3)	NOISE LVL dBA(CORR)
A4	914	77.5	0	62	1.52	.18	78.58
A5	1182	75.5	0	1.84	1.24	.13	78.71
A6	895	77.55	0	82	1.43	.15	78.31
A7	906	78	0	7	1.52	.18	79.00
A8	1191	74.4	0	1.91	1.52	.18	78.01
A9	1041	76.6	0	.63	1.52	.18	78.93
					A	JERAGE>>	78.59
					S.	TD DEV>>	0.38
					90	0% C.I.>	0.31

## TABLE XII

## FAA/GAMA PROPELLER AIRCRAFT NOISE PROGRAM

## SALINA,KS FIELD ELEVATION 1270'

AIRCRAFT: BEECH 1900

TEST DATE: 9/19/84

## REFERENCE ALTITUDE: 869'

EVENT		NOISE LVL	DELTA(M)	DELTA(1)	DELTA(2)	DELTA(3)	NOISE LVL
A10	782	80.55	0	-1.01	1.27	.2	81.01
A11	964	77.95	Ŏ	.99	.92	.2	80.06
A13	951	80.8	Ō	.86	.48	.2	82.34
A15	1028	78.75	0	1.61	.92	.23	81.51
A16	931	77.9	0	.66	.92	.23	79.71
A17	977	79.95	0	1.12	1.01	.23	82.31
					A	VERAGE>>	81.16
					S.	TD DEV>>	1.11
					90	0% C.I.>	0.91

AIRCRAFT: BEECH 1900

TEST DATE: 9/19/84

REFERENCE ALTITUDE

798.00 W/REDUCED POWER

EVENT		NOISE LVL dBA(MEAS)	DELTA(M)	DELTA(1)	DELTA(2)	DELTA(3)	NOISE LVL
B19	844.00	77.85	0.00	0.54	1.04	0.00	79.43
B20	952.00	74.80	0.00	1.69	0.85	0.00	77.34
B21	952.00	74.75	0.00	1.69	0.76	0.00	77.20
B23	948.00	75.25	0.00	1.65	0.76	0.00	77.66
B24	834.00	77.45	0.00	0.42	0.85	0.00	78.72
B25	908.00	76.25	0.00	1.23	0.76	0.00	78.24

AVERAGE>>	78.10
STD DEV>>	0.87
90% C.I.>	0.71

## TABLE XIII

## FAA/GAMA PROPELLER AIRCRAFT NOISE PROGRAM

## SALINA, KS FIELD ELEVATION 1270'

AIRCRAFT: CESSNA 402C

TEST DATE: 9/19/84

REFERENCE ALTITUDE: 846'

EVENT	MEAS.ALT AGL(ft)	NOISE LUL	DELTA(M)	DELTA(1)	DELTA(2)	DELTA(3)	NOISE LVL
A36	964	79.55	.29	1.25	,87	,2	82.16
A37	924	80	. 28	.84	.87	.2	82.19
A38	958	79.8	. 29	1.19	.87	. 2	82.35
A40	882	80.15	. 26	.4	.79	.18	81.78
A41	951	80.2	.29	1.12	.79	.18	82.58
A42	889	79.95	.27	.47	.79	.18	81.66
					A	VERAGE>>	82.12
					8.	TD DEV>>	0.35
					9	0% C.I.>	0.29

AIRCRAFT: CESSNA 402C

TEST DATE: 9/19/84

REFERENCE ALTITUDE

639.00 W/REDUCED POWER

EVENT		NOISE LVL	DELTA(M)	DELTA(1)	DELTA(2)	DELTA(3)	NOISE LUL
					~		
B45	776.00	75.10	0.39	1.86	0.70	0.00	78.05
B46	537.00	79,05	0.16	-1.66	0.79	0.00	78.34
<b>B</b> 47	677.00	76.65	0.20	0.55	0.70	0.00	78.10
<b>B</b> 48	752.00	75.80	0.23	1.56	0.70	0.00	78.29
B49	651.00	76.80	0.20	0.18	0.79	0.00	77.97
850	597.00	80.15	0.18	-0.65	0.79	0.00	80.47

AVERAGE>> 78.54 STD DEV>> 0.96 90% C.1.> 0.79

## TABLE XIV

## FAA/GAMA PROPELLER AIRCRAFT NOISE PROGRAM

## SALINA.KS FIELD ELEVATION 1270'

AIRCRAFT: PIPER NAVAJO CHIEFTAIN

TEST DATE: 9/19/84

REFERENCE ALTITUDE

810'

EVENT		NOISE LUL dBA(MEAS)	DELTA(M)	DELTA(1)	DELTA(2)	DELTA(3)	NOISE LVL dBA(CORR)
A51	915	82.45	0.27	1.16	1.40	0.32	85.81
A52	920	61.60	0.28	1.22	1.40	0.32	84.82
A53	776	82.55	0.23	-0.41	1.40	0.32	84.09
A54	934	82.30	0.28	1.36	1.40	0.32	85.66
A55	901	82.60	0.27	1.02	1.32	0.32	85.53
					AL	PERAGE>>	85.18
					ST	D DEV>>	0.72
					90	× 6.1.5	0.69

AIRCRAFT: PIPER NAVAJO CHIEFTAIN TEST DATE: 9/19/84

REFERENCE ALTITUDE 654 W/REDUCED POWER

EVERT		NJISE LUL dBA(MEAS)	DELTA(M)	DELTA(1)	DELTA(2)	DELTA(3)	NOISE LUL dBA(CORR)
857 858 860 861 862	979.00 907.00 690.00 933.00 844.00	77.85 77.50 79.55 77.40 78.60	0.29 0.27 0.21 0.28 0.25	3.85 3.12 0.51 3.39 2.44	1.37 1.37 1.46 1.37	00.0 00.0 00.0 00.0	83.36 82.26 81.73 82.44 82.66
					A	/ERAGE>>	82.49
					S.	TD DEV>>	0.60
					90	0% C.I.>	0.57

## TABLE XV

## FAA/GAMA PROPELLER AIRCRAFT NOISE PROGRAM

## SALINA.KS FIELD ELEVATION 1270'

AIRCRAFT: BEECH A-36

TEST DATE: 9/18/84

MAX.CONT.POWER AT S.L. 300 bhp

~							
A80	ALTITUDE	ALTITUDE	DENSITY	STD.TEMP	OAT	POWER AT	DELTA 3
EVENT	AGL(ft)	MSL(ft)	RATIO	DEG.F	DEG.F	ALTITUDE	DB
				~~~~			
A6	869	2139	.93889	51.4	62	276.44	0.40
A7	784	2054	.94126	51.7	62	277.31	0.58
A8	793	2063	.94101	51.6	62	277.20	0.58
A9	899	2169	.93805	51.3	62	276.13	0.51
A10	798	2048	.94087	51.6	61	277.42	0.58

AIRCRAFT: MOONEY 201

TEST DATE: 9/18/84

MAX.CONT.POWER AT S.L. 200 bhp

	ALTITUDE	ALTITUDE	DENSITY	STD.TEMP	OAT	POWER AT	DELTA 3
EVENT	AGL(ft)	MSL(ft)	RATIO	DEG.F	DEG.F	ALTITUDE	DB
A56	793	2063	.94101	51.6	68	183.77	0.62
A57	702	1972	.94355	52	68	184.40	0.60
A58	721	1991	.94302	51.9	70	183.93	0.62
A61	749	2019	.94224	51.8	70	183.73	0.63
A62	717	1987	.94313	51.9	70	183.95	0.62
A64	838	2108	.94255	51.9	70	133.90	0.62

AIRCRAFT: CESSNA 210L

TEST DATE: 9/18/84

MAX.CONT.POWER AT S.L. 285 BHP

EVENT	ALTITUDE AGL(ft)	4LTITUDE MSL(ft)	DENSITY RATIO	STD.TEMP DEG.F	DEG.F	POWER AT ALTITUDE	DELTA 3
A80 •	714	1984	.94322	51.9	75	260.95	0.65
A81	724	1994	.94294	51.9	75	260.86	0.65
A83	553	1823	.94774	52.5	75	262.53	0.61
A84	736	2006	.9426	51.8	75	260.73	0.66
A85	672	1942	.94439	52.1	75	261.37	0.54
A86	675	1945	.94431	52.1	76	261.10	≎.⊝5

APPENDIX A

METEOROLOGICAL DATA

TABLE A1

FAA/GAMA PROPELLER AIRCRAFT
NOISE PROGRAM

SALINA MUNICIPAL AIRPORT

TEST DATE: 9/18/84

	BAR. PRESS.	TEMP.	REL.HUMID.	WIND AT	lom.
TIME	In.Hg.	Deg F	Percent	SPEED(mph)	DIR
7:30	30.25	49.8	8.8	0.5	SE
7:44		50.6	8.8	1.0	SE
8:32	30.27	53.6	8.8	3.0	SE
8:43		54.6	8.8	3.0	SE
9:01		54.3	84	2.5	SE
7:38	30.27	60.1	74	4.0	SSE
7:58		42.7	70	3.0	8
10:10		62.4	66	4.0	SSE
10:29	30.28	43.1	62	5.5	SSE
11:16		66.4	57	7.0	SE
11.38	30.26	67.6	54	6.0	SSE
12:02		71.5	48	11.0	SSE
12:31	30.24	74.5	46	5.5	. 8
1:30	30.23	76.4	42	4.5	SSE
1:49		77.4	42	8.0	SSE
2:09	30.22	77.7	38	4.5	SSE
2:37		76.6	36	4.0	SE
3:40	30.17	77.6	44	10.0	SE
3:59		77.8	38	7.0	SE
4:18	30.18	79.7	38	4.0	SE
4:57	30.16	79.8	38	7.0	ESE
5;21		79.9	40	8.0	SE
5:40		80.2	40	6.0	ESE

TABLE A2

FAA/GAMA PROPELLER AIRCRAFT

NOISE PROGRAM

SALIN	A MUNICIPAL AI	RPORT	TEST D	ATE: 9/19/8	4
	BAR.PRESS.	TEMP.	REL.HUMID.	WIND AT	10m.
TIME	In.Hg.	Deg F	Percent	SPEED(mph)	DIR
7:40	30.15	55.0	86	2.0	SE
8:13		56.7	73	2.0	SE
8:34		59.8	81	1.0	SE
9:24	30.16	61.0	47	4.0	SSE
9:46		64.0	60	5.0	SSE
10:07		48.0	52	4.5	SSE
10:21		71.8	50	7.0	SSE
10:29		74.1	49	4.0	SSE
11:09		78.5	34	11.5	SSE
11:33	30.14	82.5		4 . 5	S
12:06		84.0	30	8.0	SSE
12:46		87.1	28	8.0	SE
1:18		87.4	28	8.0	SE
1:31		88.4	25	8.0	ESE
1:51		88.2	2 4	6.0	SSE
4:23	30.01	88.0	25	10.0	SE
4:36		88.1	2 3	12.0	SE
4:54		88.8	22	10.0	382
5:10		87.7	2 2	10.0	SE
5 23		87.5	? 2	14.0	SE

APPENDIX B

#### TABLE B1

#### FAA/GAMA PROPELLER AIRCRAFT NOISE PROGRAM

AIRCRAFT: BEECH A-36 TEST DATE: 9/18/84

#### COCKPIT DATA

	VIDECTAPE			FLIGHT ENGINEER'S LOG		
EVENT	TIME	I AS Knots	ALTITUDE OVER MIC	MANIFORD PRESSURE	PROP RPM	OAT DEG F
A6	7:55:51	100	860	27.5	2700	62
A7	8:04:45	102	770	27.5	2700	62
AS	8:22:31	103	780	27.5	2700	62
A9	8:28:21	100	820	27.5	2700	62
A10	8:31:41	102	780	27.5	2700	61
Bii	8:36:45	105	480	27.5	2400	61
812	8:42:48	103	520	28.0	2400	60
B13	8:46:16		690	28.0	2400	61
B14	8:49:50	100	680	28.0	2400	61
B15	8:53:44	101	760	28.0	2400	61
B16	8:57:04	101	680	28.0	2400	61

#### TABLE B2

#### FAA/GAMA PROPELLER AIRCRAFT NOISE PROGRAM

AIRCRAFT: MOONEY 231 TEST DATE: 9/18/84

		VIDEOTAPE		FLIGHT ENGINEER'S LOG		
EVENT	TIME	IAS Knots	ALTITUDE OVER MIC	MANIFORD PRESSURE	PROP RPM	OAT DEG C
A23	9:54:36	97	670	40.0	2695	1 2
A24	9:57:55	95	680	40.0	2695	12
A25	10:01:06	97	800	39.8	2695	12
A26	10:04:01	97	800	40.0	2695	12
A27	10:07:08	97	790	37.8	2695	12
A28	10:10:11	97	790	39.8	2695	12
829	10:13:45	95	630	35.0	2400	13
<b>B</b> 30	10:16:45	95	590	35.2	2400	13
<b>B</b> 31	10:19:54	95	640	35.2	2400	13
<b>B</b> 32	10:22:50	95	570 .	35.0	2400	13
B33	10:27:07	95	640	35.0	2400	13
834	10:32:14	95	700	35.0	2400	14

TABLE B3

#### FAA/GAMA PROPELLER AIRCRAFT NOISE PROGRAM

AIRCRAFT: SENECA III

TEST DATE: 9/18/84 C SERIES: 9/19/84

		VIDEOTAPE	FLIGHT ENGINEER'S LOG				
EVENT	TIME	IAS Knots	ALTITUDE OVER MIC	maniford Pressure	PROP RPM	OAT Deg f	
A37			770	40.0			
A38	11:32:26	90	880	40.0	2600	62	
A39	11:37:33	72	880	40.0	2600	62	
A 4 0	11:42:29	91	880	40.0	2600	62	
A41	11:46:57	91	920	40.0	2600	62	
A42	11:51:37	90	900	40.0	2600	43	
B47	12:16:28	95	710	34.0	2400	63	
B48	12:21:10	93	710	34.0	2400	63	
B49	12:25:47	90	730	33.5	2400	63	
B50	12:30:30	92	680	33.5	2400	63	
B51	12:35:20	90	700	34.0	2400	63	
B5 2	12:40:33	92	700	34.0	2400	63	
C26	11:09:01	92	820	40.0	2800	75	
C27	11:13:55	93	880	40.0	2800	75	
C 2 8	11:19:00	90	900	40.0	2800	75	
C29	11:23:43	90	890	40.0	2800	75	
C30	11:28:23	90	960	40.0	2800	75	
C31	11:32:56	90	820	40.0	2800	75	

#### TABLE B4

#### FAA/GAMA PROPELLER AIRCRAFT NOISE PROGRAM

AIRCRAFT: MOONEY 201 TEST DATE: 9/18/84

ENT TIME

162 1:57:33 164 2:03:01

174 2:31:49

376 2:37:49

377 2:39:24

378 2:42:15

1:40:29

1:43:46

1:46:32 1:54:55

2:09:19

2:23:24

88

89

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87

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161

366

371

COCKPIT DATA

VIDEOTAPE		FLIGHT E	NG INEER'S	LOG	
IAS	ALTITUDE	MANIFORD	PROP	OAT	-
Knots	OVER MIC	PRESSURE	RPM	DEG	C
					-
8 7	770	27.5	2700	20	
8 9	700	28.0	2700	20	
87	700	28.0	2700	2 1	
8.8	730	28.0	2700	2 1	
87	700	28.0	2700	2 1	
	800	28.0	2700	2 1	

27.5

28.0

28.0

28.0 28.0

28.0

2400

2400

2400

2400

2400

2400

2 1

2 1

21

2 1

21

21

#### TABLE BS

670

610

670

640

690

480

#### FAA/GAMA PROPELLER AIRCRAFT NOISE PROGRAM

AIRCRAFT: CESSNA 210L TEST DATE: 9/18/84

	VIDEOTAPE			FLIGHT ENGINEER'S LOG		
		IAS	ALTITUDE	MAN1 FORD	PROP	DAT
VENT	TIME	Knots	OVER MIC	PRESSURE	RPM	DEG F
A80	3:43:29	97	680	F.T.	2700	75
A81	3:44:58	9 6	740	F.T.	2700	75
A83	3:55:36	97	570	F.T.	2700	75
A84	3:59:19	97	710	F.T.	2700	75
A85	4:03:08	. 98	660	F.T.	2700	75
A 8 6	4:06:30	98	660	F.T.	2700	76
887	4:10:28	97	640	F.T.	2400	76
B88	4:14:19	97	690	F.T.	2400	76
B 8 9	4:18:21	98	610	F.T.	2400	76
B90	4:22:10	97	680	F.T.	2400	76
B 9 1	4:25:33	97	540	F.T.	2400	76
B 7 2	4:28:45	98	700	F.T.	2400	76

TABLE B6

B106 5:45:46

λ9

8:40:18

#### FAA/GAMA PROPELLER AIRCRAFT NOISE PROGRAM

AIRCRAFT: BEECH 58TC TEST DATE: 9/18/84

			COCKPIT DAT	Ά		
		VIDEOTAPE		FLIGHT EN	GINEER'S	LOG
		IAS	ALTITUDE	MANIFORD	PROP	OAT
EVENT	TIME	Knots	OVER MIC	PRESSURE	RPM	DEG F
A93	4:58:19	115	770	39.5	2685	78
A 9 4	5:01:47	112	820	39.5	2685	78
A95	5:05:56	111	780	39.5	2685	78
A96	5:08:04	114	880	39.5	2685	78
A97	5:11:11	113	840	39.5	2685	78
A 9 8	5:14:39	115	730	39.5	2685	78
B100	5:24:00	116	720	36.5	2400	78
B101	5:27:35	115	680	36.5	2400	78
B103	5:34:13	117	720	36.5	2400	78
B104	5:39:55	115	680	36.5	2406	78
B105	5:42:30	115	540	36.5	2400	78

TABLE B7

750

113

105

36.5

32.5

78

72

2370

2400

#### FAA/GAMA PROPELLER AIRCRAFT NOISE PROGRAM

AIRCRAFT: CESSNA T303 TEST DATE: 9/19/84

#### COCKPIT DATA VIDEOTAPE FLIGHT ENGINEER'S LOG ALTITUDE MANIFORD PROP OAT IAS RPM DEG F OVER MIC PRESSURE EVENT TIME Knots ----72 8:12:36 105 840 32.5 2370 **A4** 68 1050 32.5 2370 8:17:29 105 A5 32.5 2370 70 8:22:46 105 820 λó λ7 8:28:14 105 840 32.5 2370 72 2370 72 8:33:42 102 1060 32.5 λB

940

#### TABLE B8

#### FAA/GAMA PROPELLER AIRCRAFT NOISE PROGRAM

AIRCRAFT: BEECH 1900 TEST DATE: 9/19/84

COCKPIT	DATA
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VIDEOTAPE		FLIGHT EN	LOC			
EVENT	TIME	I AS Knots	ALTITUDE OVER MIC	TORQUE	PROP RPM	OAT DEG C
A10	9:23:30	138	770	3400	1690	23
A11	9:28:32	140	840	3400	1700	23
A13	9:36:53	145	850	3400	1700	23
A15	9:45:42	140	880	3400	1700	24
A16	9:49:37	138	840	3400	1700	24
A17	9:53 28	135	870	3400	1700	24
B19	10:02:16	140	820	3400	1550	24
B20	10:07:14	135	870	3400	1550	23
B21	10:11:48	137	880	3400	1550	22
B 2 3	10:20:35	140	870	3400	1550	23
B24	10:24:39	140	770	3400	1550	23
B25	10:28:42	137	• 840	3400	1550	23

#### TABLE B9

#### FAA/GAMA PROPELLER AIRCRAFT NOISE PROGRAM

AIRCRAFT: CESSNA 402C TEST DATE: 9/19/84

			COCKETT DAT			
		VIDEOTAPE	1	FLIGHT EN	IG INEER'S	LOG
EVENT	TIME	I AS Knots	ALTITUDE OVER MIC	MANIFORD PRESSURE	PROP RPM ·	OAT DEG C
<b>A36</b>				39.0	2700	23
A37				39.0	2700	23
A 3 B				39.0	2700	23
A40	1:18:00	110	840	40.0	2700	22
A41	1:21:03	110	930	40.0	2700	22
A 4 2	1:24:24	110	880	40.0	2700	22
B45	1:34:02	110	780	29.5	2450	2 1
B46	1:37:00	110	570	29.5	2450	22
B47	1:39:59	110	710	29.5	2450	21
B48	1:43:12	110	780	29.5	2450	2 1
B49	1:47:05	110	650	29.5	2450	22
B50	1:50:52	110	620	29.5	2450	22

TABLE B10

#### FAA/GAMA PROPELLER AIRCRAFT NOISE PROGRAM

AIRCRAFT: PIPER NAVAJO CHIEFTAIN TEST DATE: 9/19/84

	VIDEOTAPE			FLIGHT ENGINEER'S LOG		
EVENT	TIME	I AS Knots	ALTITUDE OVER MIC	MANIFORD PRESSURE	PROP RPM	OAT DEG F
A51	4:31:04	107	820	49.0	2560	82
A52	4:36:20	105	840	49.0	2560	82
A53	4:41:03	107	700	49.0	2560	82
A54	4 : 45 : 48	104	840	49.0	2560	82
A55	4:50:14	105	780	49.0	2560	82
A54	4:55:49	104	1020	49.0	2560	81
B5 7	5:01;34	110	890	40.0	2400	81
B58	5:06:09	112	820	40.0	2400	81
B60	5:14:55	113	640	40.0	2400	82
B61	5:19:38	113	840	40.0	2400	8 1
B62	5:24:08	111	790	40.0	2400	81

A MANAGEMENT AND A CONTRACTOR OF THE CONTRACTOR

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>72 PUR PLANT RPRS: RAJOR
>73 SOTTLE STYGENS MONE
>74 BULK STYGENS HIGH
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DIS RAMAGER: JOHN F SCANLON
DIS ADDRESS: HUNICIPAL ARPT
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DIS PHONE HRS 913-627-3910
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                 16 AIRPORT USE: PUBLIC
19 ARPT LAT: 38-47-29-7N SURVETED
28 ARPT LONG: 897-39-62-34
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22 ACREAGE: 2734
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               22 ACREAGE: 2734
PR3 RIGHT TRAFFIC:
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               DEA NON-COMM LANDING FEEL NO
28 NASP/FEDERAL AGREEMENT: NAPRY
26 FAR 139 INDEX: AASSS/73
                                                                                                                                                                               87 FSS ON ARPTI YES
88 FSS PHONE MR: 913-625-8984
89 TOLL FREE MR;
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MOS EMDING SEJUHAS
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RWY 60 /22 RWY 4-22 CHTR 75° ASPH GVERLAT.

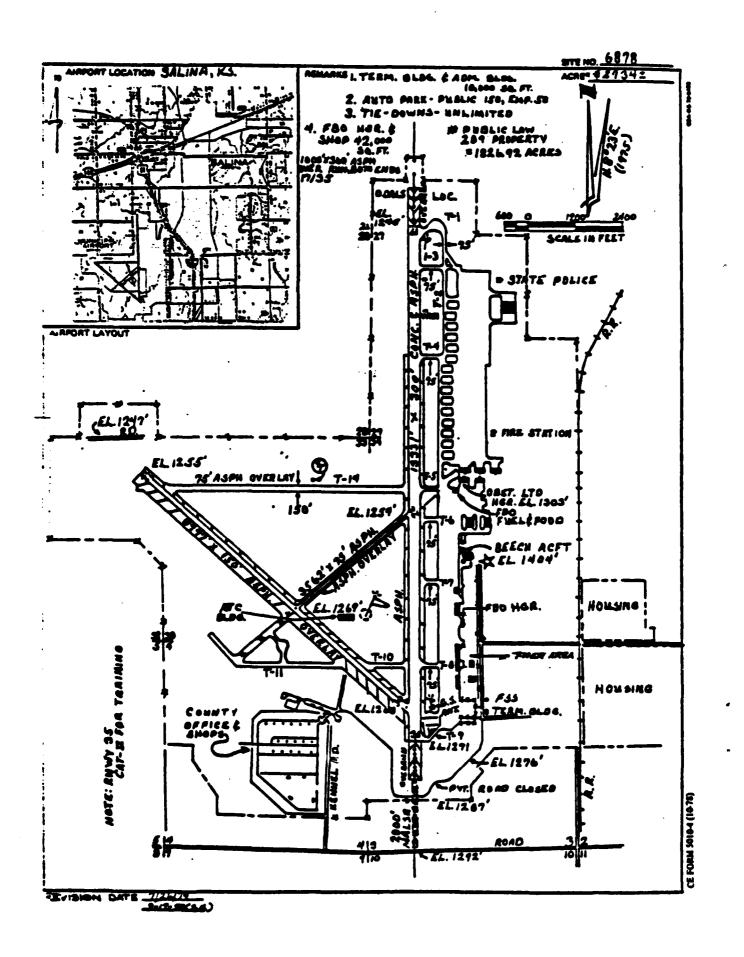
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ROTO BEN LETD AT 38-47-22.1M 897-38-21.8W

RWY 4-22 STW STRENSTHMS FOR CHTR 79° ASPH GVERLAY: 8-188. 9-138 & 97-238.

TWY 6 APRON FAIR COND.

INTO-PLAME CONTRACT FUEL A NOT AVAILABLE.
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## FILMED

7-85

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